# **Flow Rate Calculations**

- using orifice plates -

## Liquid Flow Rate

The basic formula for liquid flow rate in gph is:

$$gph = \sqrt{(h_w) * F_b * F_{gt} * F_r * F_a}$$

where:

 $\mathbf{h}_{w}$  = differential pressure across the orifice plate (in inches of water)

 $\mathbf{F}_{\mathbf{b}}$  = basic orifice factor

**F**<sub>gt</sub> = gravity temperature factor

 $\mathbf{F}_{\mathbf{r}} = \text{Reynolds number}$ 

 $\mathbf{F}_{a}$  = orifice thermal expansion factor

If the calculation is not being used for custody transfer or accounting, the last two terms can eliminated without much error.

#### Hot Oil Loop Setup:

The following assumptions have been made for the hot oil loop at the Thermal Oxidizer:

*Line size*: 8" schedule 80, which translates to 7.625" ID. *Orifice plate bore*: 5.9996" diameter. *Hot oil line dP transmitter is scaled*: 0-200" wc. *Specific gravity*: 0.87. *Flowing temperature*: 350°F. *Pressure*: 70-85 psig.

 $\mathbf{h_w}$  = measured from the dP transmitter.  $\mathbf{F_b}$  = 9075.9 (this number is estimated from fig 3-16 in the GPSA Engineering Data Book. According to this table, the existing orifice plate is too large to yield accurate measurement. The largest plate that should be used is 5.5".)  $\mathbf{F_{at}}$  = 1.0057/ $\sqrt{(0.87)}$  = 1.078 Some error will be introduced because we do not know the

 $F_{gt} = 1.005/(\sqrt{(0.87)}) = 1.078$  Some error will be introduced because we do not know the specific gravity at the flowing temperature.

**gpm** = gph/60.

So the formula which is used in the PLC is:

**gpm** = (9075.9) \* (1.078) \*  $\sqrt{(dP)} / 60$ . **gpm** = 163.1  $\sqrt{(dP)}$ .

This is calculated on rung 60:98 in the thermal oxidizer Process PLC.

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## **Gas Flow Rate**

The basic formula for gas flow rate in scfh is:

scfh = 
$$\sqrt{hw} * \sqrt{P_f} * F_b * F_{pb} * F_{tf} * F_{pv} * F_g * F_r * Y * F_{th} * F_a$$

where:

- $\mathbf{h}_{w}$  = differential pressure across the orifice plate (in inches of water)
- $\mathbf{P}_{\mathbf{f}}$  = static pressure, psia
- $\mathbf{F}_{\mathbf{b}}$  = basic orifice factor
- $\mathbf{F}_{\mathbf{pb}}$  = pressure base factor
- $\mathbf{F}_{tf}$  = flowing temperature factor
- $\mathbf{F}_{pv}$  = supercompressibility factor
- $\mathbf{F}_{g}$  = specific gravity factor
- $\mathbf{F}_{\mathbf{r}} = \text{Reynolds number}$
- **Y** = expansion factor
- $\mathbf{F}_{th}$  = temperature base factor
- $\mathbf{F}_{\mathbf{a}}$  = orifice thermal expansion factor

If the calculation is not being used for custody transfer or accounting, the last four terms can eliminated without much error.

#### Amine Tail Gas Loop:

The following assumptions have been made:

*Line size*: 6" schedule 80, which translates to 5.761" ID. *Orifice plate bore*: 2.817" diameter. *Tail gas dP transmitter is scaled*: 0-75" wc. *Tail gas pressure transmitter is scaled*: 0-50 psig. *Specific gravity*: 1.5075. *Flowing temperature*: 87°F.

$$\begin{split} & h_w = \text{measured from the dP transmitter.} \\ & P_f = \text{measured from the pressure transmitter, psig + 14.7 to convert to psia.} \\ & F_b = 1666.7 \text{ (interpolated from fig 3-16 in the GPSA Engineering Data Book).} \\ & F_{pb} = 1 \text{ (we are at sea level, so no correction is required).} \\ & F_{tf} = \sqrt{[520/(460+T_f)]} \text{ where } T_f \text{ is the flowing temp, = 0.9750.} \text{ This equation converts to} \\ & \text{ an absolute temperature scale.} \\ & F_{pv} = \text{Unknown. Assume = 1.} \\ & F_a = \sqrt{[1/G]}, \text{ where } G \text{ is the specific gravity, = 0.8145.} \\ & \text{mcfd} = \text{scfh} * 24 \text{ hrs/day} * 1 \text{ mcf/1000 scf} = 0.024 \text{ scfh.} \\ & \text{mcfd} = 31.77 * \sqrt{hw} * \sqrt{P_f} \end{aligned}$$

This is calculated in file 24 of the Thermal Oxidizer Process PLC.